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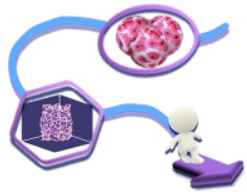
Centro E. Piaggio
bioengineering and robotics research center

INGEGNERIA DEI TESSUTI BIOLOGICI: DYNAMIC MECHANICAL ANALYSIS (DMA)

Giorgio Mattei

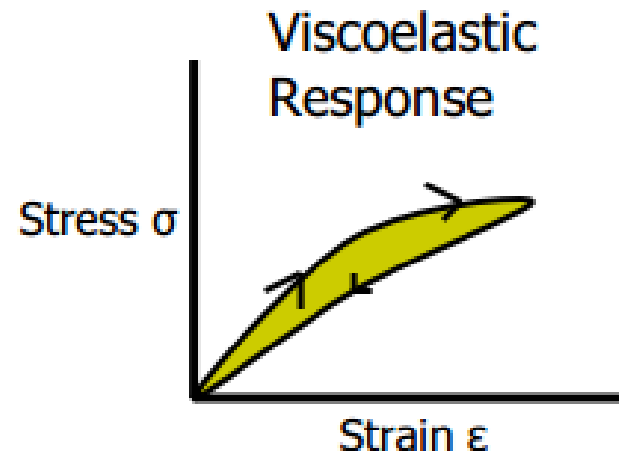
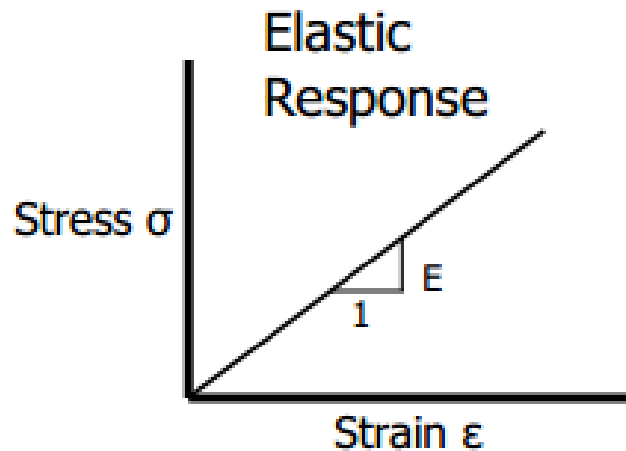
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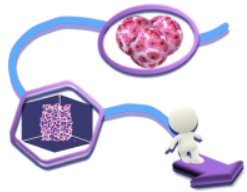
18 April 2016



Viscoelasticity

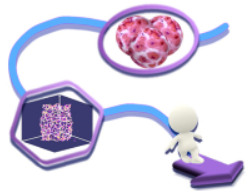
- **Viscoelastic materials** exhibit the characteristics of both elastic and viscous materials
 - Viscosity \rightarrow resistance to flow (damping)
 - Elasticity \rightarrow ability to revert back to the original shape
- **Elastic vs. viscoelastic** stress-strain response





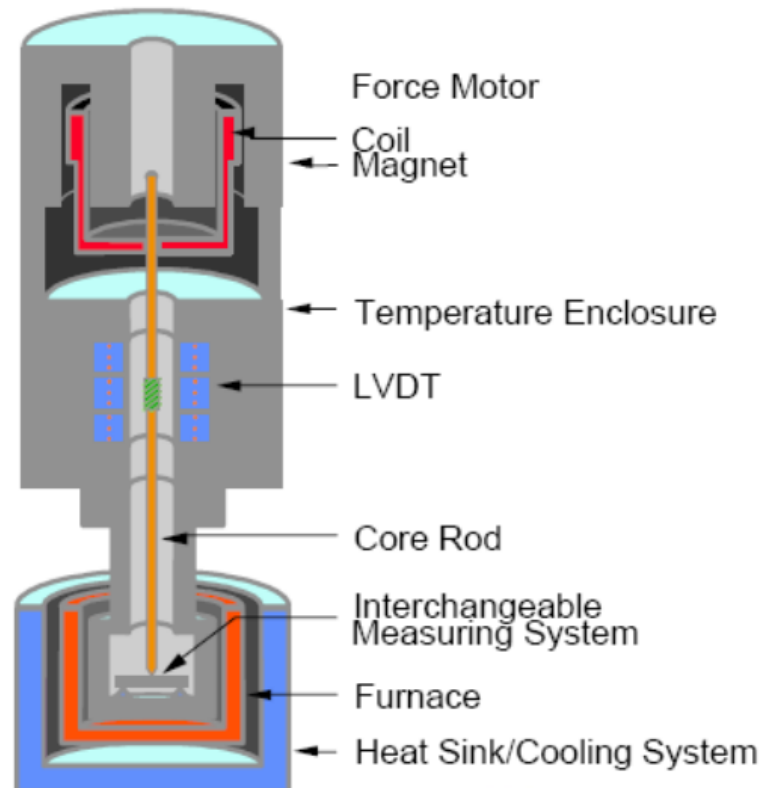
Methods to characterise viscoelasticity

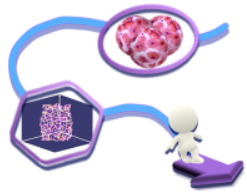
- **Time domain**
 - Creep response
 - Stress relaxation
 - Epsilon dot Method ($\dot{\epsilon}M$, Tirella A. et al., JBMR 2013)
- **Frequency domain**
 - Dynamic mechanical analysis (DMA)
 - Dynamic mechanical thermal analysis (DMTA)



DMA overview

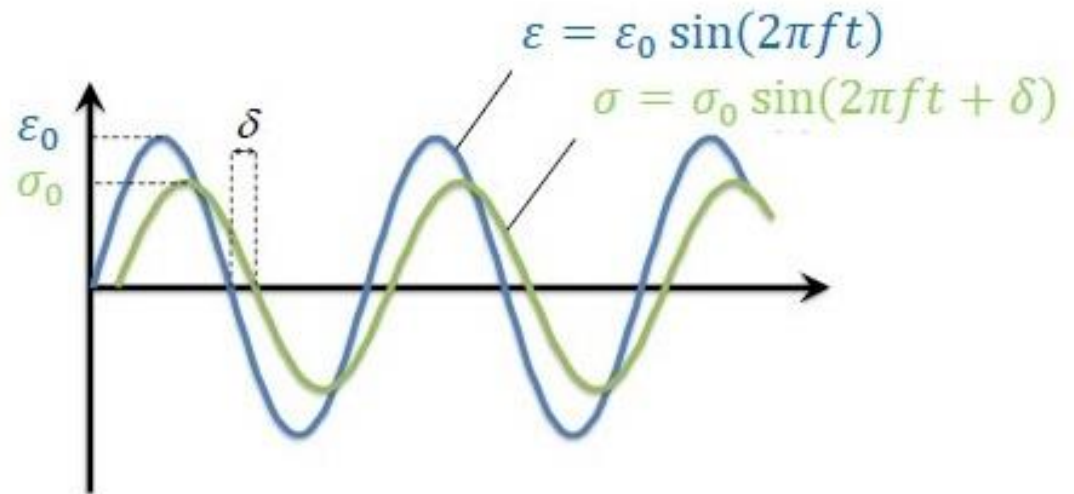
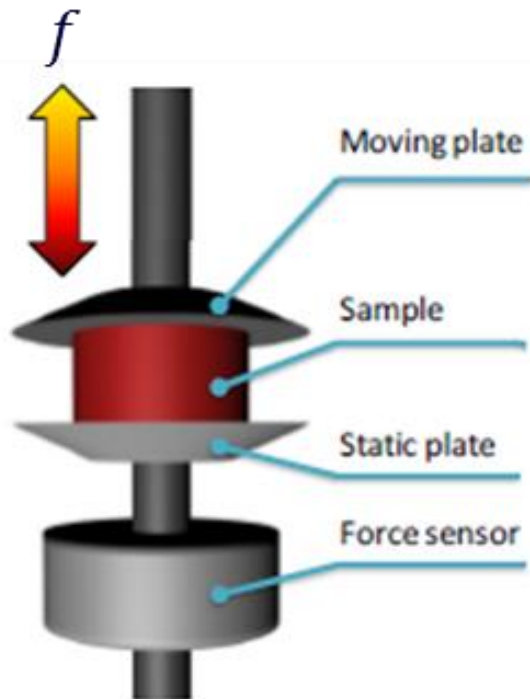
- Dynamic mechanical analysis (DMA) is a standard **force-triggered method** to **determine viscoelastic properties** of materials by **applying a small amplitude cyclic strain** on a sample and **measuring the resultant cyclic stress response**.



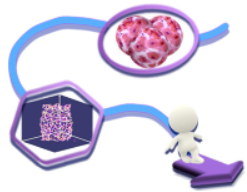


DMA overview

- For a given **sinusoidal strain input** the resulting **stress will be sinusoidal** if the **applied strain is small enough** so that the tissue can be approximated as linearly viscoelastic.

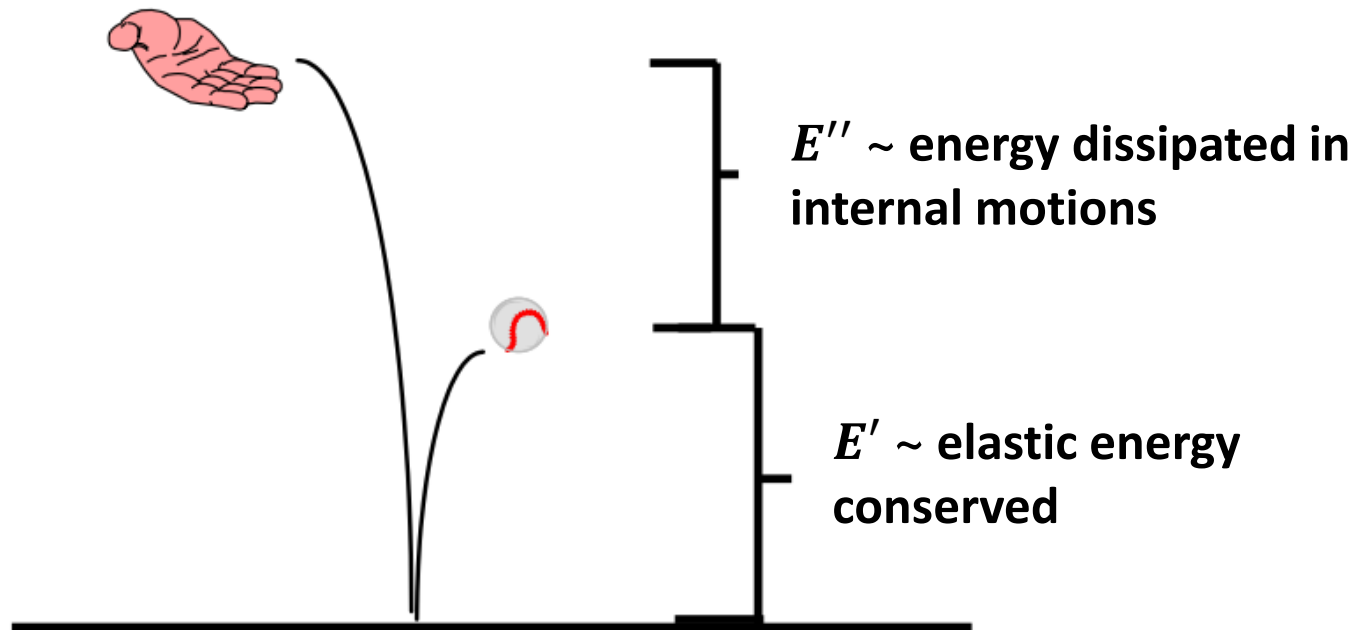


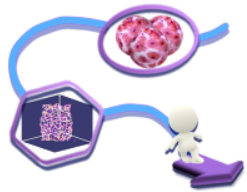
Viscoelastic material response is characterised by a **phase lag (δ)** between the strain input and the stress response, which is comprised **between 0° (purely elastic) and 90° (purely viscous)**. This phase lag is **due to the excess time necessary for molecular motions and relaxations** to occur.



Complex, storage and loss modulus

- The dynamic mechanical properties are quantified with the **complex modulus** (E^*), which can be thought as an **overall resistance** to deformation under dynamic loading. The complex modulus is composed of the **storage** (E' , elastic component) and the **loss** (E'' , viscous component) moduli, that are **additive under the linear theory of viscoelasticity** ($E^* = E' + iE''$).

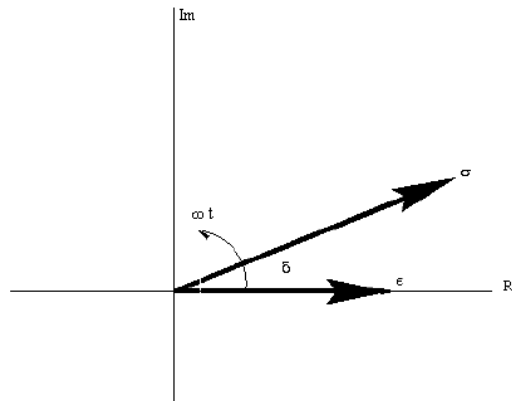
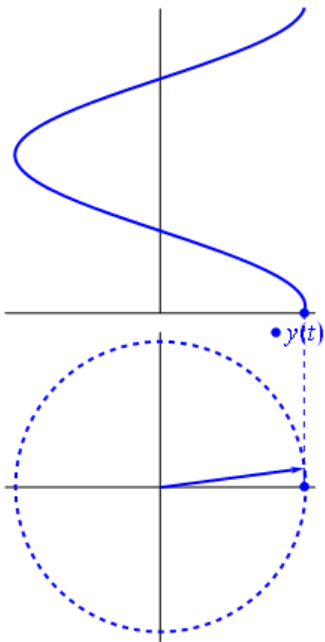




Definitions

- It is convenient to represent the sinusoidal stress and strain functions as complex quantities (called rotating vectors, or **phasors**) with a **phase shift** of δ .

$$\varepsilon = \varepsilon_0 e^{i\omega t} \quad \sigma = \sigma_0 e^{i(\omega t + \delta)}$$



Observable σ and ε can be viewed as the projection on the real axis of vectors rotating in the complex plane at the same frequency ω

Rotating vector representation of harmonic stress and strain

$$\begin{aligned} E^* &= \frac{\sigma}{\varepsilon} = \frac{\sigma_0}{\varepsilon_0} e^{i\delta} = \\ &= \frac{\sigma_0}{\varepsilon_0} (\cos \delta + i \sin \delta) = \\ &= E' + iE'' \end{aligned}$$

Storage modulus

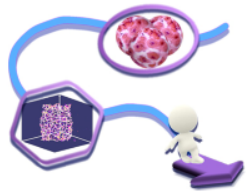
$$E' = E^* \cos(\delta)$$

Loss modulus

$$E'' = E^* \sin(\delta)$$

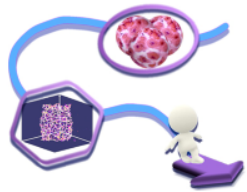
$$\tan(\delta) = E''/E' \quad \text{Damping factor}$$

$$\eta' = E''/\omega \quad \text{Dynamic viscosity}$$



Test modes

- **Temperature sweep:** Modulus and damping are recorded as the sample is heated
- **Frequency sweep:** Modulus and damping are recorded as the sample is loaded at increasing (or decreasing) frequencies
- **Stress amplitude sweep:** Modulus and damping are recorded as the sample stress is increased
- **Strain amplitude sweep:** Modulus and damping are recorded as the sample strain is increased
- **Combined sweep:** Combinations of above methods

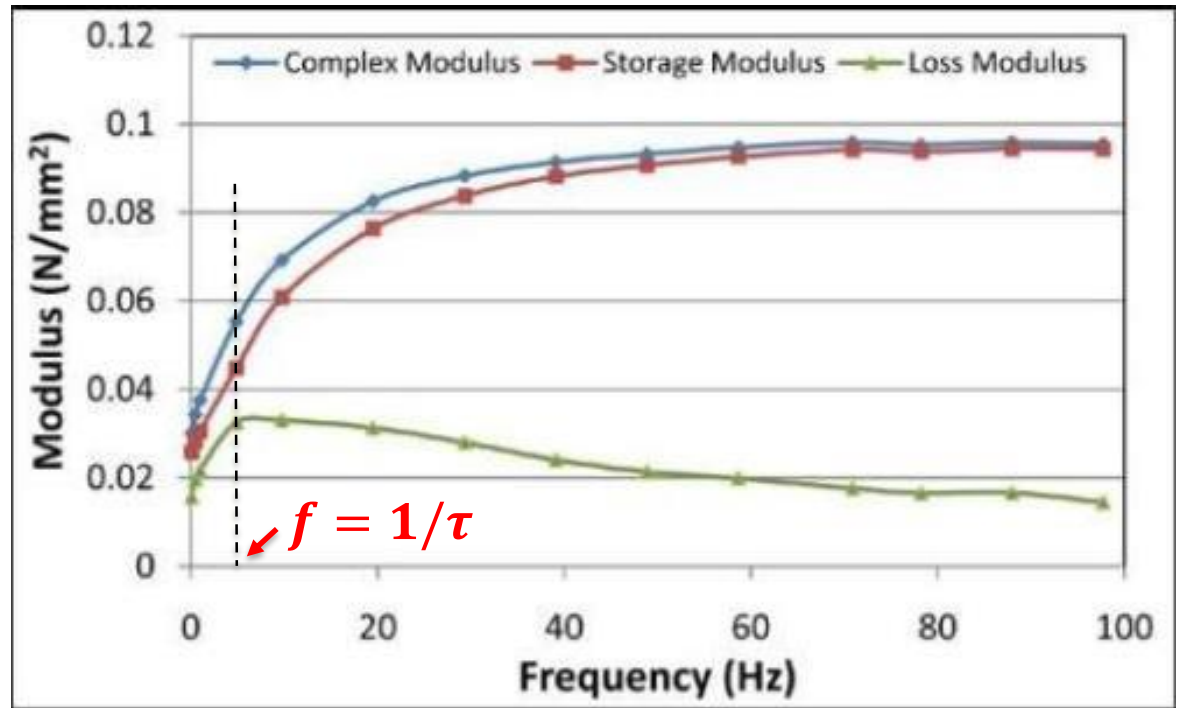
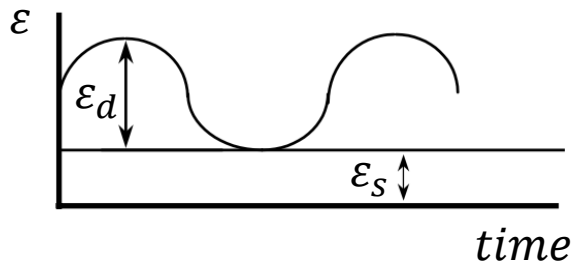


Frequency sweep tests

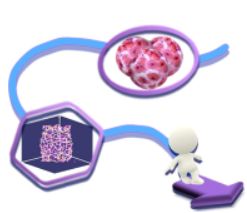
- A sample is held to a **fixed temperature** and tested at **varying frequency**.

Test parameters:

- Temperature (T)
- Frequency range (f)
- Static strain (ϵ_s)
- Dynamic strain (ϵ_d)

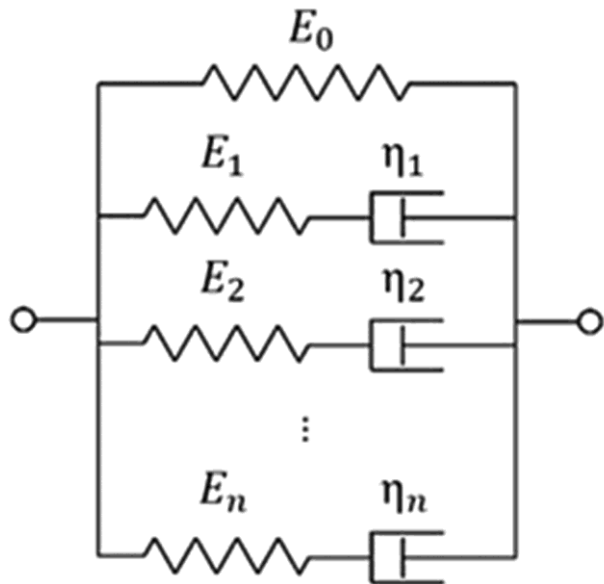


- Peaks** in $\tan(\delta)$ or E'' with respect to frequency identify the **characteristic relaxation frequencies** of the viscoelastic sample under testing, defined as $f = 1/\tau$, where τ is the **characteristic relaxation time**)



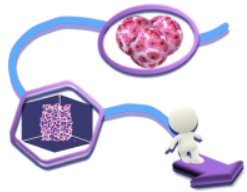
Lumped models to describe material linear viscoelastic response

- The most general form of linear viscoelastic model is called the **Generalised Maxwell (GM)** model and consists of a **pure spring (E_0)** with **n Maxwell arms** (i.e. spring E_i in series with a dashpot η_i) assembled **in parallel**, thus defining a set of **n different characteristic relaxation times** (i.e. $\tau_i = \eta_i/E_i$)



$$H_{GM}(s) = \frac{\bar{\sigma}}{\bar{\epsilon}} = E_0 + \sum_{i=1}^n \frac{E_i \eta_i s}{E_i + \eta_i s}$$

GM model transfer function in the Laplace domain

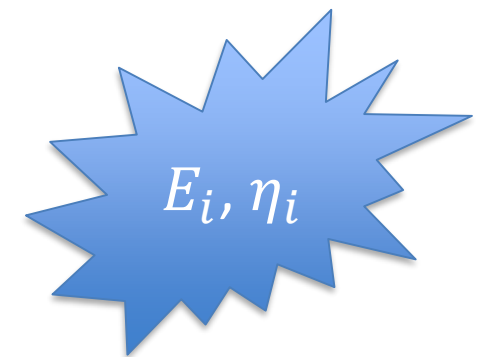
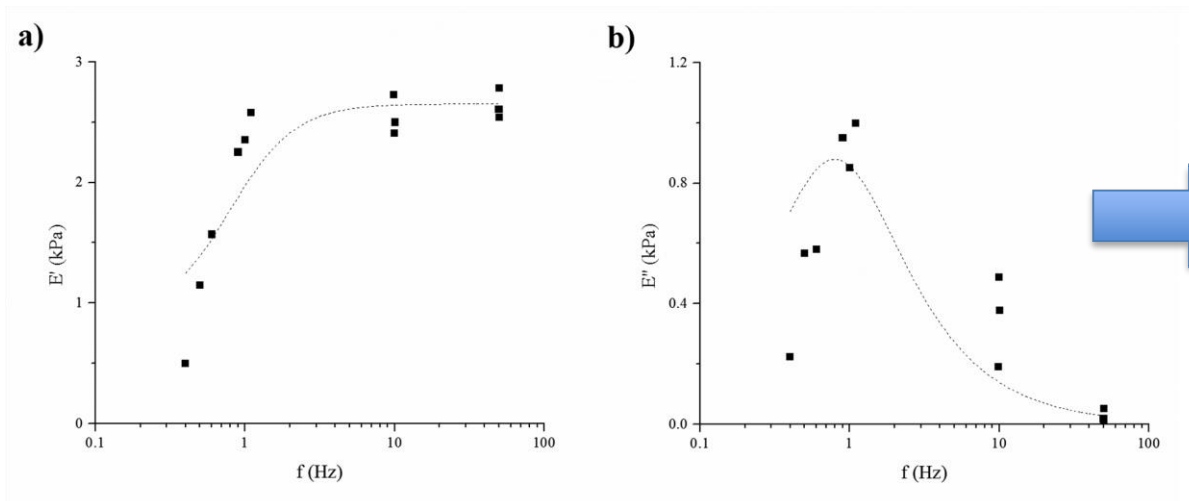



Lumped parameters derivation from frequency sweep tests

- Calculate the **complex conjugate of the GM modulus** (E_{GM}^*) by substituting $s = i \omega = i 2\pi f$ in $H_{GM}(s)$, then **split the expression into its real (Re)** and **imaginary (Im)** parts to obtain the **frequency-dependent relations** for the **storage** and **loss** moduli, respectively

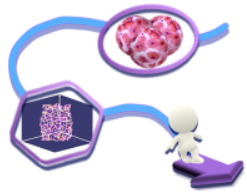
$$E_{GM}^*(f) = \underbrace{\left(E_0 + \sum_{i=1}^n \frac{4 E_i \eta_i^2 f^2 \pi^2}{E_i^2 + 4 \eta_i^2 f^2 \pi^2} \right)}_{E'(f)} + i \underbrace{\left(\sum_{i=1}^n \frac{2 E_i^2 \eta_i f \pi}{E_i^2 + 4 \eta_i^2 f^2 \pi^2} \right)}_{E''(f)}$$

- Global fitting with shared parameters** (χ^2 minimisation)

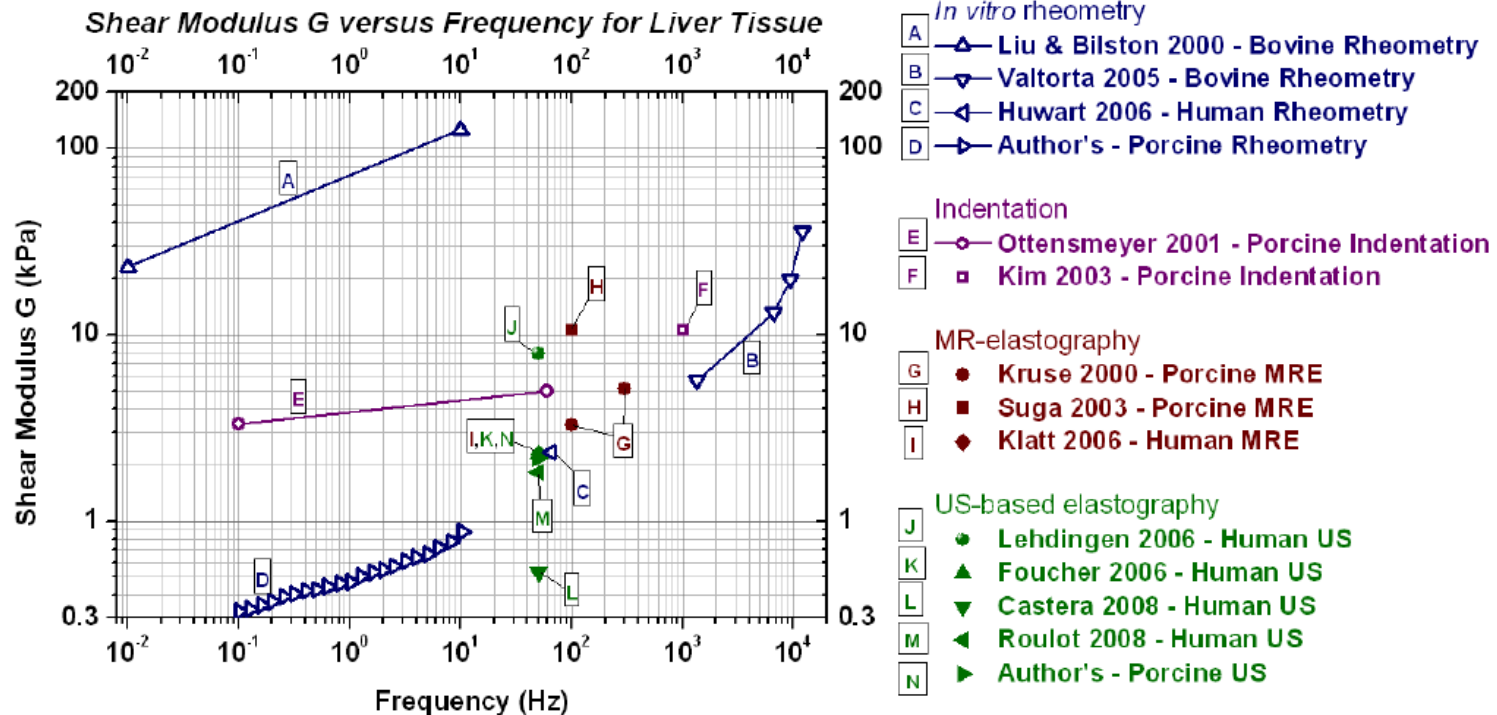




CASE OF STUDY: THE LIVER



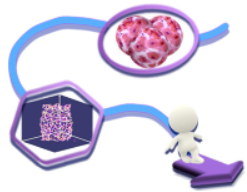
SoA: a myriad of different results



Source: S. Marchesseau et al., *Progress in biophysics and molecular biology*, 103:2–3, pp. 185–96, 2010



Many **variables and factors** affect measured liver mechanical properties, leading to a lack of consensus and unique properties, which are **critical for developing appropriate viscoelastic models**



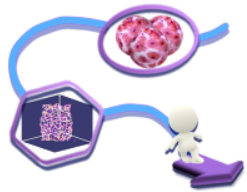
Typical variability factors

- **Testing condition**
 - *in-vivo*: tissue in its **natural state**, but many **testing limitations**
 - *ex-vivo*: better for **developing testing devices, protocols and tissue models**
- **Testing method and experimental setup**
 - Direct measurements or image-based techniques
 - Time, strain rate or frequency range considered
- **Tissue sample**
 - **Type and source**: animal source, presence of Glisson's capsule
 - **Status**: environmental testing parameters, physical conditions, post-mortem time, preservation period, pathophysiological state, preload



From this multifaceted research area emerges **the need to:**

1. **clearly identify the parameters of interest**
2. **develop suitable experimental testing setup and protocols for the unique identification of liver viscoelastic parameters**

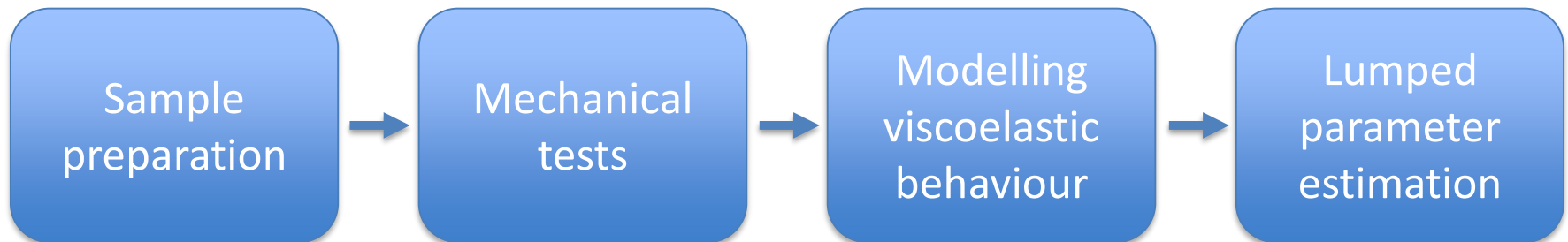


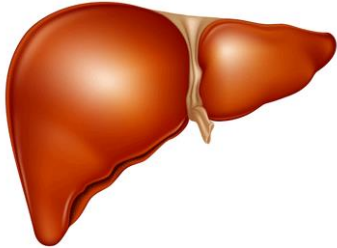
Aim and strategy

AIM: establishing an **experimental testing and analysis framework** to **unequivocally** characterise the **liver viscoelastic behaviour** in the **LVR** (linear viscoelastic region)

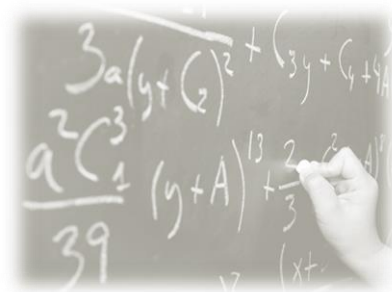
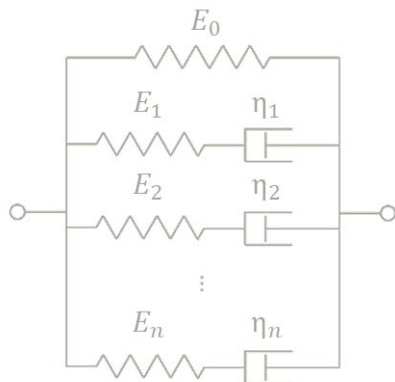
STRATEGY: *ex-vivo* measurements in **unconfined compression** using **common testing apparatus** and **2 different testing methods**

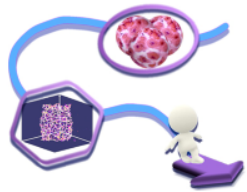
- **ϵM** , a solution to **avoid major drawbacks** of force- or strain-triggered methods in **testing floppy samples** (e.g. **long test duration** and significant **sample pre-load**)
- **step-reconstructed DMA**, a modification of a **widely used technique** for viscoelastic characterisation of materials





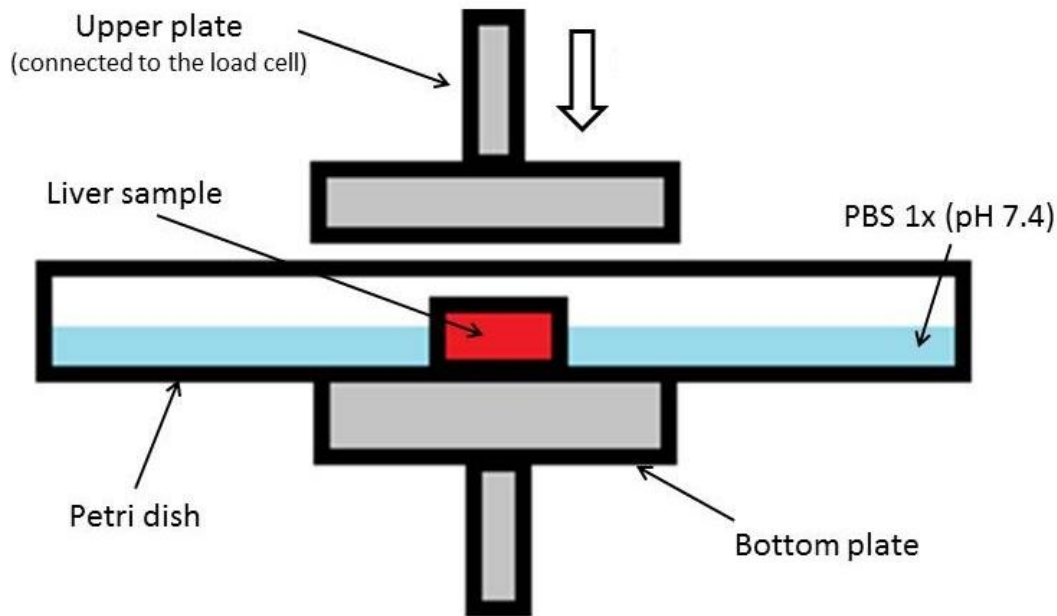
Sample preparation



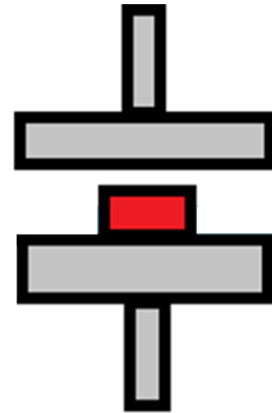
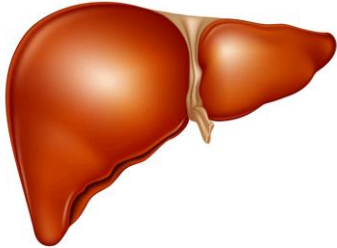


Sample preparation and testing configuration

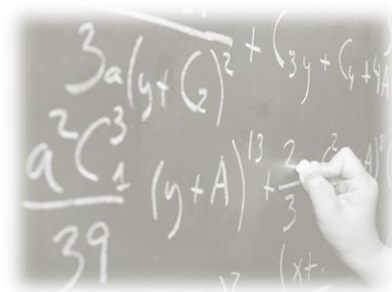
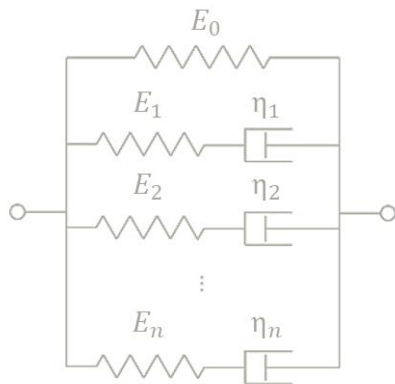
- **Cylindrical liver samples** (14 mm diameter, 3 mm thickness) collected from **1 year old healthy pigs avoiding Glisson's capsule and macroscopic vasculature**
- **Repeatable testing condition** → samples **equilibrium swollen in PBS 1x at 4°C**, then **brought to room T** and **carefully measured** prior testing

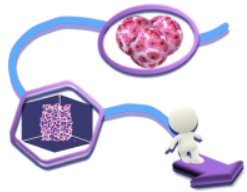


Testing configuration



Mechanical tests

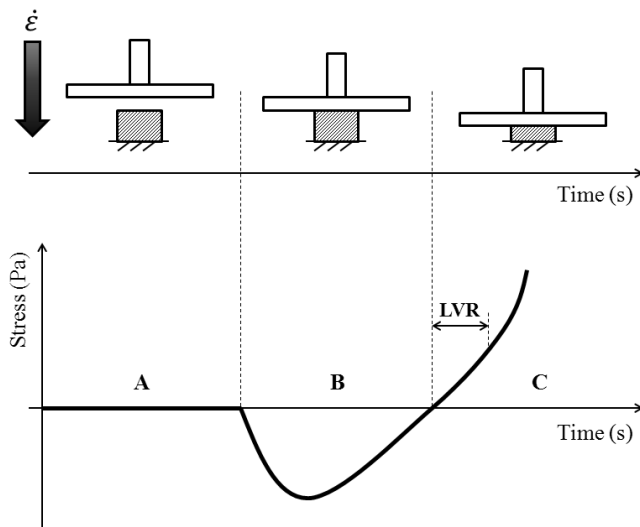




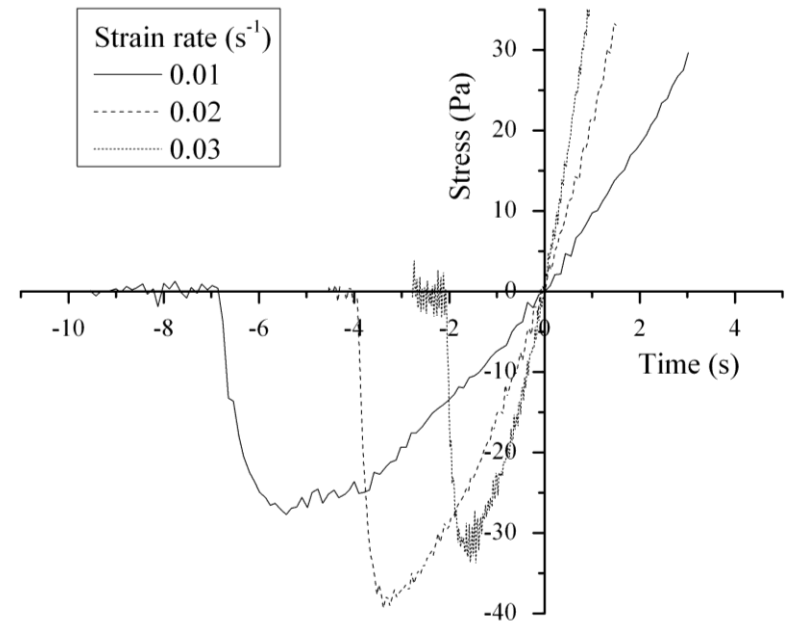
$\dot{\epsilon}M$: short test with no pre-load

A. Tirella, G. Mattei, A. Ahluwalia, JBMR Part A (2013)

$\dot{\epsilon}M$ paradigm: characterise the material viscoelastic behaviour testing samples at different constant strain rates ($\dot{\epsilon}$), then analysing $\sigma(t)$ curves



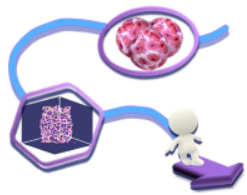
- ✓ Implementable with **all uniaxial testing devices**
- ✓ **Force-displacement time recording** starts **prior to sample contact** → **no pre-load**
- ✓ **Short test duration** → **no sample deterioration**
- ✓ **LVR** determined through **measured σ - ϵ curves**
- x Need **preliminary tests** or an **a priori knowledge of the material relaxation behaviour** to choose $\dot{\epsilon}$



Experimental stress-time data at various $\dot{\epsilon}$
(only **LVR values** are shown in zone C)

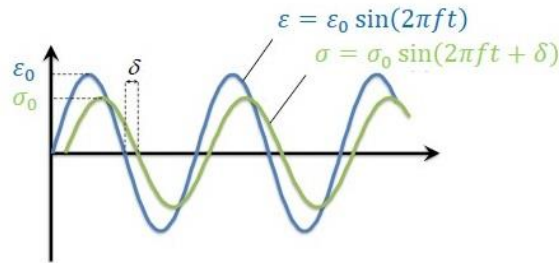
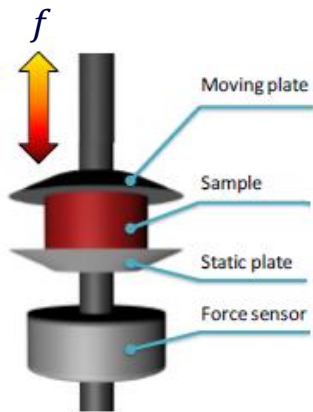
Zwick/Roell 2005, 10N load cell

3 samples x 3 $\dot{\epsilon}$ = 9 samples



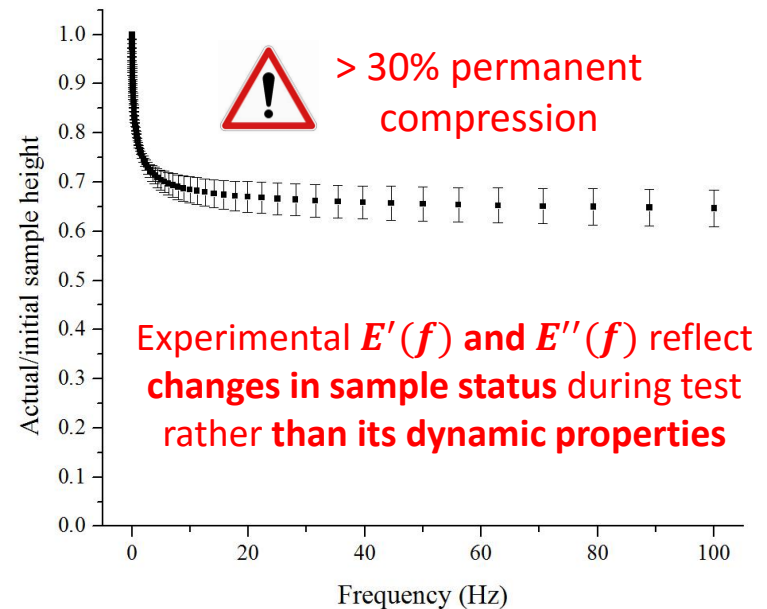
DMA: a widely accepted method

DMA paradigm: characterise viscoelastic behaviour testing samples at **different frequencies (f)**, then analysing **$E'(f)$ and $E''(f)$**



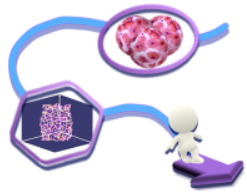
$$E' = \frac{\sigma_0}{\varepsilon_0} \cos(\delta) \quad E'' = \frac{\sigma_0}{\varepsilon_0} \sin(\delta) \quad E^* = E' + iE''$$

- ✓ Largely accepted for viscoelastic characterisation
- ✓ Wide frequency sweep tests **simplify testing set-up** avoiding preliminary tests or any *a priori* knowledge
- x Long testing time may **degrade the sample**
- x Trigger force may **significantly pre-load samples**
- x Preliminary strain-sweep tests to **derive the LVR**



Permanent deformation during a 0.05 – 100 Hz frequency sweep test (~ 1.5 h)

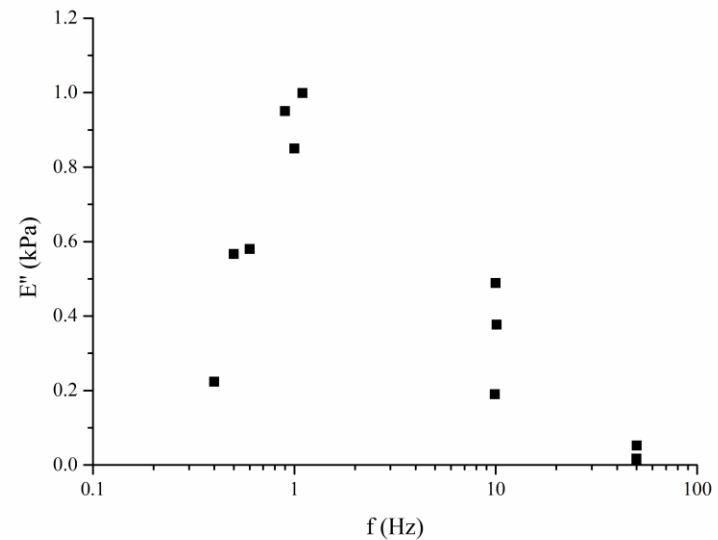
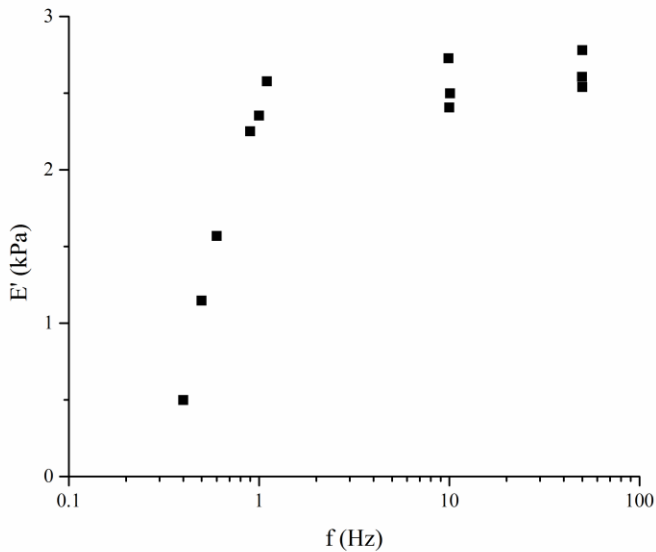
GABO Eplexor 150N, 10mN trigger force
3 samples



step-reconstructed (SRDMA)

G. Mattei, A. Tirella, G. Gallone, A. Ahluwalia, *submitted*

SRDMA paradigm: perform **DMA** measurements around specific f , then reconstruct $E'(f)$ and $E''(f)$ over the whole frequency range of interest

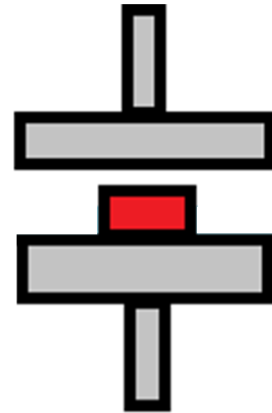
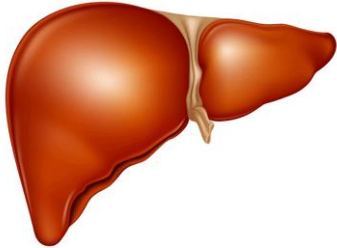


Storage (E') and loss (E'') moduli measured around $f = 0.5, 1, 10$ and 50 Hz ($f - 0.1$ Hz, f , $f + 0.1$ Hz)

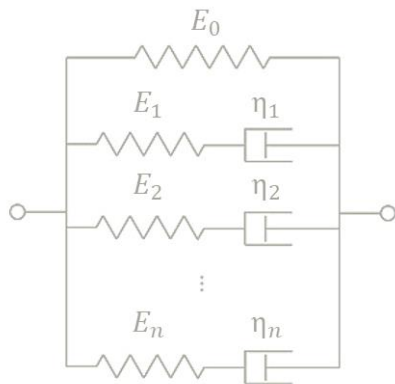
GABO Eplexor 150N, 10mN trigger force

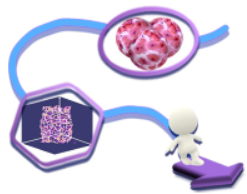
3 samples \times 4 f = 12 samples

- ✓ **Short testing time** \rightarrow **no sample deterioration** (< 2 % permanent compression in the *worst* case, i.e. $f = 0.5$ Hz)
- x **Trigger force** \rightarrow **sample pre-load**
- x Need **preliminary tests** or an ***a priori* knowledge of the material relaxation behaviour** to choose f

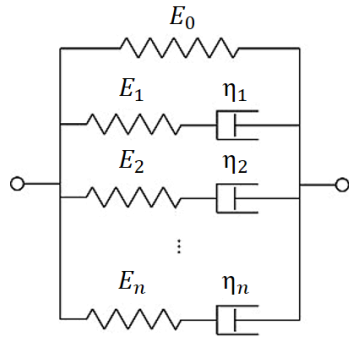


Modelling viscoelastic behaviour





Generalised Maxwell (GM) model



$$\tau_i = \eta_i / E_i \quad i^{th} \text{ relaxation time}$$

$$H_{GM}(s) = \frac{\bar{\sigma}}{\bar{\epsilon}} = E_0 + \sum_{i=1}^n \frac{E_i \eta_i s}{E_i + \eta_i s}$$

Transfer function in the **Laplace** domain

$\dot{\epsilon}M$ needs $\sigma(t)$ response to a fixed $\dot{\epsilon}$

SRDMA needs $E'(f)$ and $E''(f)$

General form

$$\bar{\sigma} = H_{GM}(s) \cdot \left(\frac{|\dot{\epsilon}|}{s^2} \right)$$

Laplace transform of a constant $\dot{\epsilon}$ input with amplitude $|\dot{\epsilon}|$

Inverse Laplace transformation

$$E_{GM}^*(f) = \underbrace{\left(E_0 + \sum_{i=1}^n \frac{4 E_i \eta_i^2 f^2 \pi^2}{E_i^2 + 4 \eta_i^2 f^2 \pi^2} \right)}_{E'(f)} + i \underbrace{\left(\sum_{i=1}^n \frac{2 E_i^2 \eta_i f \pi}{E_i^2 + 4 \eta_i^2 f^2 \pi^2} \right)}_{E''(f)}$$

**Max SLS
($n = 1$)**

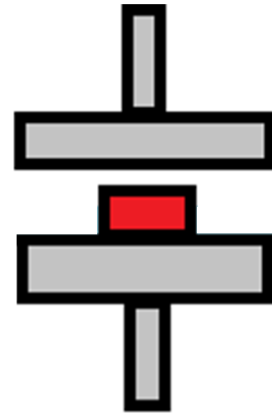
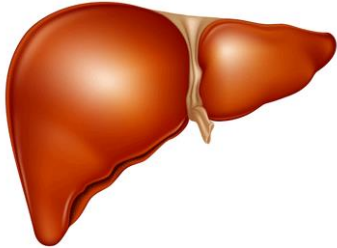
$$\sigma(t) = \dot{\epsilon} \left[E_0 t + \eta_1 \left(1 - e^{-\frac{E_1}{\eta_1} t} \right) \right]$$

substitute **$n = 1$** in the general equation

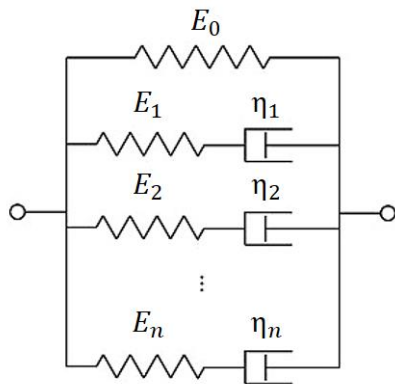
**GM2
($n = 2$)**

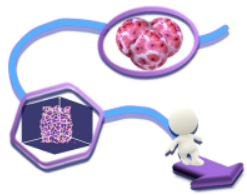
$$\sigma(t) = \dot{\epsilon} \left[E_0 t + \eta_1 \left(1 - e^{-\frac{E_1}{\eta_1} t} \right) + \eta_2 \left(1 - e^{-\frac{E_2}{\eta_2} t} \right) \right]$$

substitute **$n = 2$** in the general equation



Lumped parameter estimation





Global fitting with shared parameters

$\dot{\epsilon}M$

SRDMA

1. Choose a lumped parameter model

2. Calculate $\sigma(t)$ response to a fixed $\dot{\epsilon}$

2. Calculate $E'(f)$ and $E''(f)$

3. Build a unique dataset for the global fit and share the viscoelastic parameters

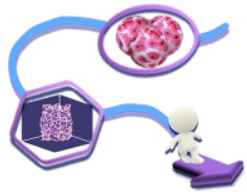
4. Fix $\dot{\epsilon}$ in the fitting equation of each experimental $\sigma(t)$ to the applied $\dot{\epsilon}$

4. Associate exp. data to the modelled expressions of $E'(f)$ and $E''(f)$

5. Global fit performing χ^2 minimisation in a combined parameter space

Annealing scheme
to avoid most of the local
minima

Viscoelastic constants (E_i, η_i) for the chosen model



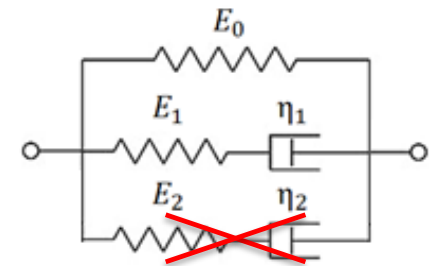
Global fitting results

Porcine liver viscoelastic parameters (estimated value \pm standard error)

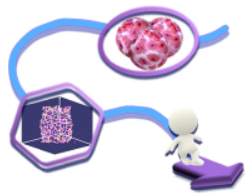
Parameter	Maxwell SLS		GM2	
	$\dot{\epsilon}M$	SRDMA	$\dot{\epsilon}M$	SRDMA
E_{inst} (kPa)	2.04 ± 0.01	2.65 ± 0.30	$2.04 \pm (3.21 \cdot 10^2) \text{ n.s.}$	$2.65 \pm (3.61 \cdot 10^5) \text{ n.s.}$
E_{eq} (kPa)	0.91 ± 0.01	0.89 ± 0.22	0.91 ± 0.01	0.89 ± 0.56
τ_1 (s)	1.10 ± 0.02	0.20 ± 0.06	$1.10 \pm (3.05 \cdot 10^3) \text{ n.s.}$	$0.20 \pm (1.14 \cdot 10^5) \text{ n.s.}$
τ_2 (s)	-	-	$1.10 \pm (3.05 \cdot 10^3) \text{ n.s.}$	$0.20 \pm (0.65 \cdot 10^5) \text{ n.s.}$
R^2	0.97	0.92	0.97	0.92

n.s. \rightarrow non significant estimate

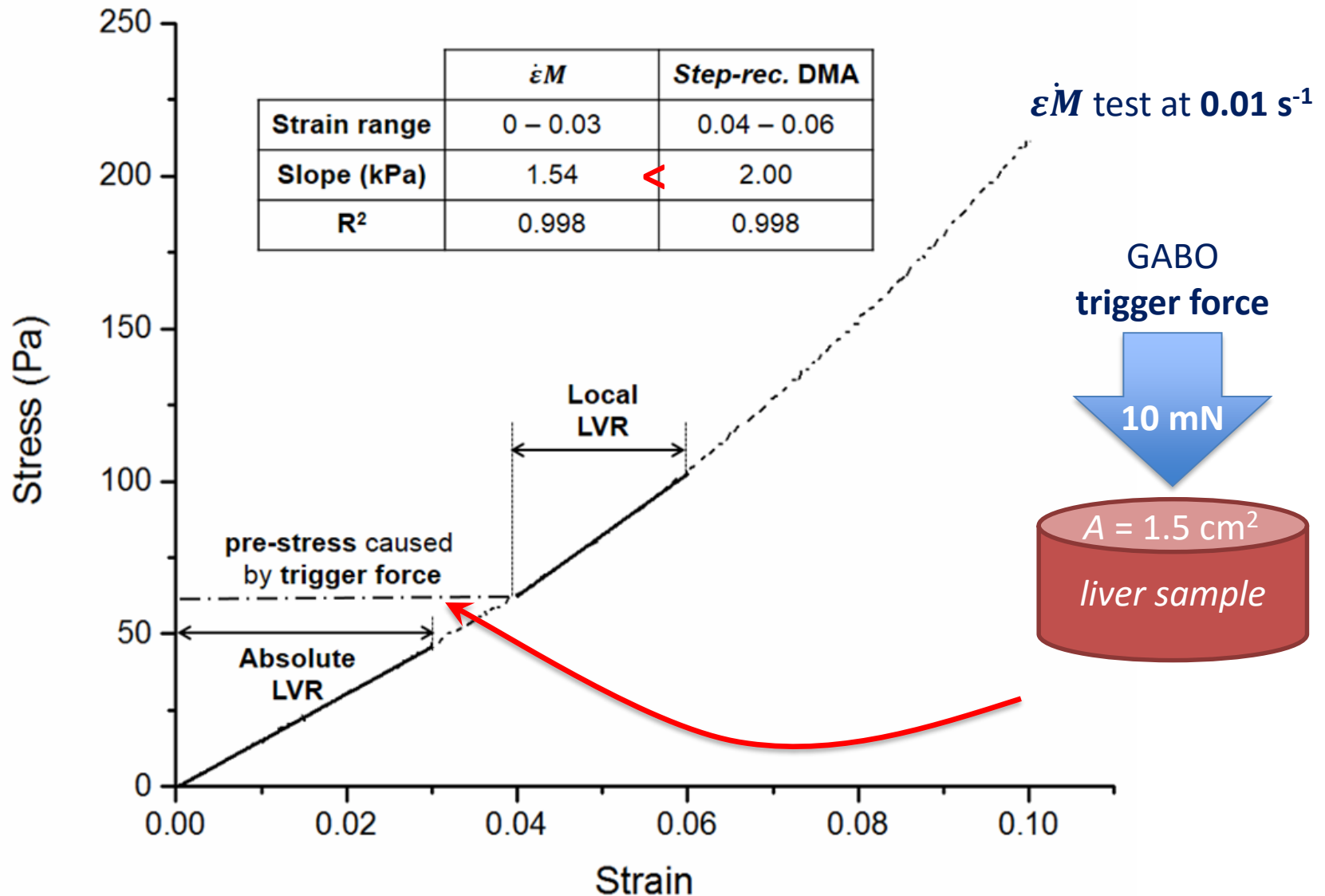
- ✓ **Maxwell SLS model is sufficient** whatever the method
- ✓ **GM2 \rightarrow over-parameterisation** of liver viscoelastic behaviour

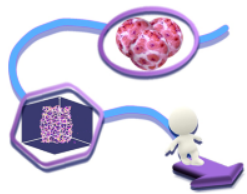


$\dot{\epsilon}M$ and SRDMA results are significantly different (t -test, $p < 0.05$)



Absolute vs local LVR





Testing very soft tissues: conclusion

Long test

F or strain trigger



sample status changes
conventional DMA

Short test

F or strain trigger



local LVR
step-rec. DMA

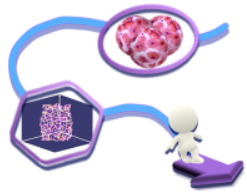
Short test

No trigger



actual properties
 $\epsilon \dot{M}$

- $\epsilon \dot{M}$ gives a **good estimation** of liver viscoelastic parameters in the LVR
- A **wider range** of $\dot{\epsilon}$ should be considered for a **more accurate estimation** of τ
- Caution in **over-interpreting *ex-vivo* data** (sample **status** is generally **different** than *in-vivo* and **dependent on many factors**, such as T, preservation period)



Contacts

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